



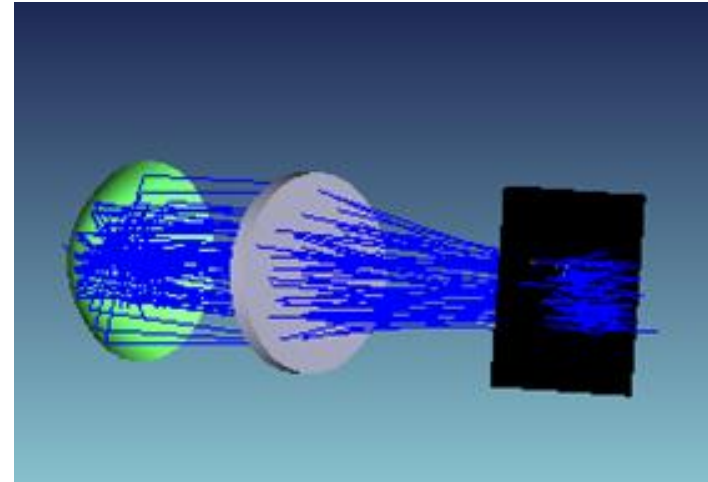
Lectures Notes on Optical Design using Zemax OpticStudio

Lecture 21

Introduction to Non-Sequential Mode in Zemax

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- 2. Sequential vs Non-Sequential Modes**
- 3. Some NSC Applications**

Introduction

There are 2 distinct ray-tracing modes in Zemax (OpticStudio)

- Sequential
- Non-sequential

In addition, a **hybrid mode** exists in which sequential and non-sequential ray-trace are used in the same system.

In this lecture, we will see some basic applications of Non-sequential ray tracing in Zemax.

Sequential Mode

- It is mainly used for designing imaging and afocal systems.
- Surfaces are defined in the Lens Data Editor.
- Ray can only intersect each surface once and has to do it in a specified -sequential- order (i.e. surface #0 then #1 ,#2 ...) and hence the name sequential ray tracing.
- Ray can only reflect if the surface material type is MIRROR. *Partial reflections from refractive surfaces (Fresnel reflections) are accounted for to the extent of calculating the correct refracted energy, including the effects on dielectric or metallic mirrors.*
- Each surface has its own local coordinate system. The position of each surface along the optical axis is referenced to the previous surface. In other words, the “Thickness” column in the Lens Data Editor refers to the distance from current surface and not from a global reference point.

Non-sequential Mode

- It is primarily used for non-imaging applications such as illumination systems and/or stray-light analysis.
- Surfaces or volume objects are defined in the Non-Sequential Component Editor
- Mechanical components may be easily imported from CAD programs, so that full Opto-Mechanical analysis may be undertaken.
- A ray can intersect the same object more than once and can intersect multiple objects in any order; hence the name non-sequential.
- Each object is referenced to a global coordinate, unless specified otherwise.
- Imaging-system properties such as stop location, entrance and exit pupil, field, system aperture etc. that exist in sequential systems may not be meaningful in non-sequential systems.
- The main analysis feature in non-sequential mode is the detector ray-trace, which gives spatial and angular data on incoherent or coherent rays.



Stray ray example

Example 1: How to add standart lens

Object Type	Comment	Ref Object	Inside Of	X Position	Y Position	Z Position	Tilt About X	Tilt About Y	Tilt About Z	Material	X Half Width	Y Half Width	# X Pixels	# Y Pixels	Data Type	Color
1 Source Ellipse ▾		0	0	0.000	0.000	0.000	0.000	0.000	0.000	-	20	1E+05	1.000	0	0	12.000
2 Standard Lens ▾		0	0	0.000	0.000	20.000	0.000	0.000	0.000	BK7	100.000	0.000	20.000	20.000	6.000	-80.000
3 Detector Rectangle ▾		0	0	0.000	0.000	120.000 V	0.000	0.000	0.000		20.000	20.000	100	100	0	3

*** Object1

Source Ellipse

of Layout Rays 20

of Analysis Rays 1e5

X Half Width 12

Y Half Width 12

*** Object2

Standart Lens

Z position 20

Material BK7

Radius1 100

Thickness 6

Clear1 = Edge1 20

Radius2 -80

Clear2 = Edge2 20

*** Object3

Detector Rect

Z position 120

Material Blank (or can be ABSORB or MIRROR)

X Half Width 20

Y Half Width 20

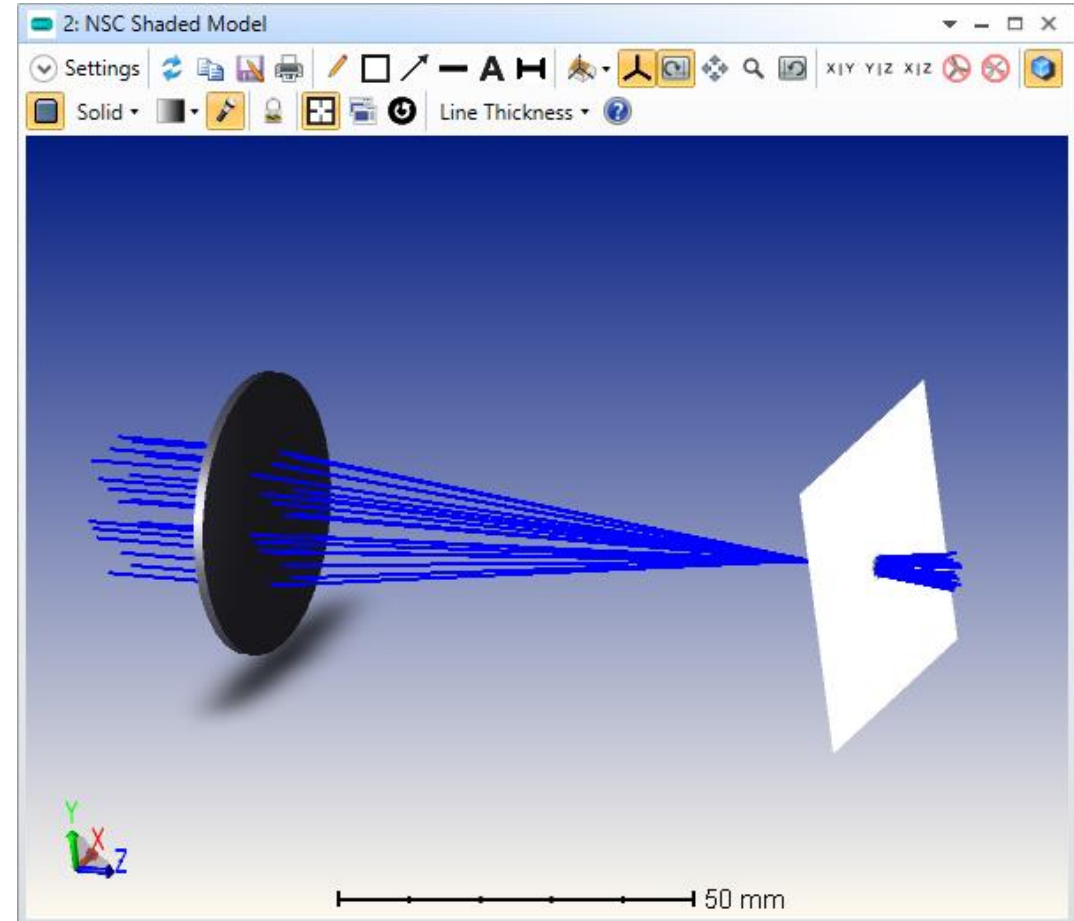
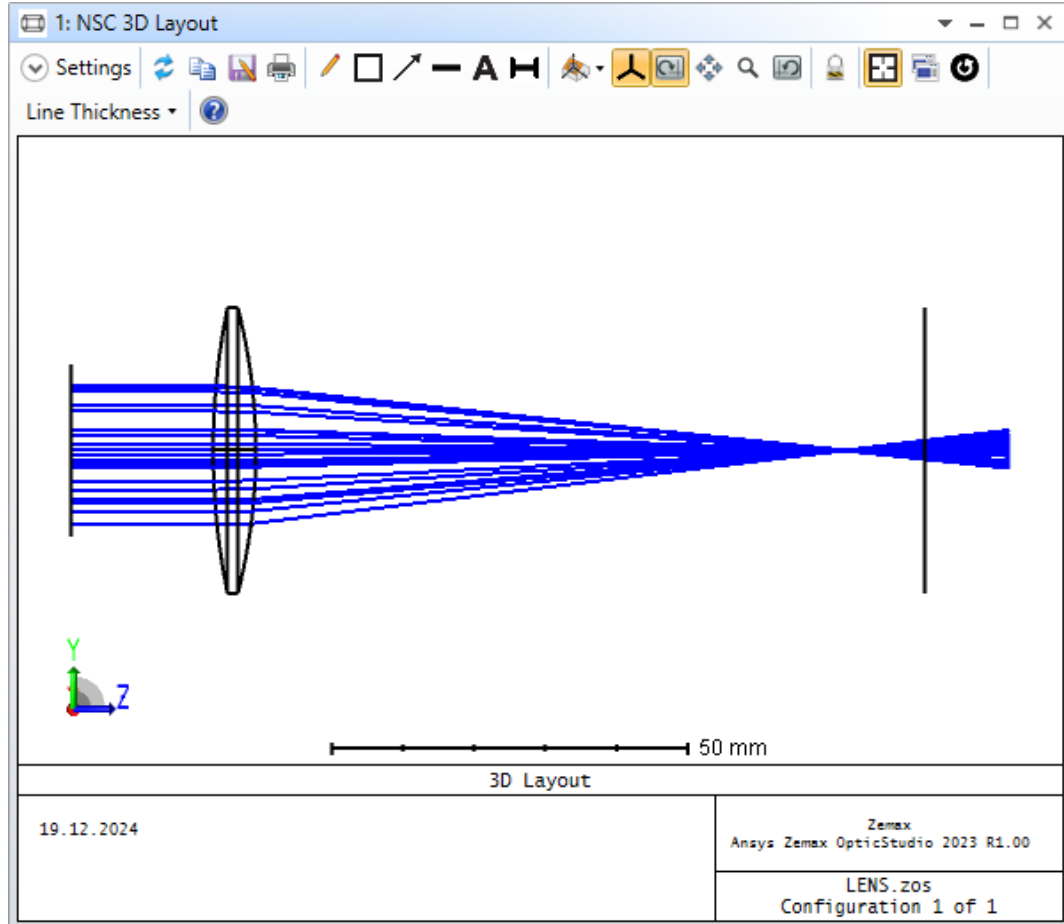
X Pixels 200

Y Pixels 200

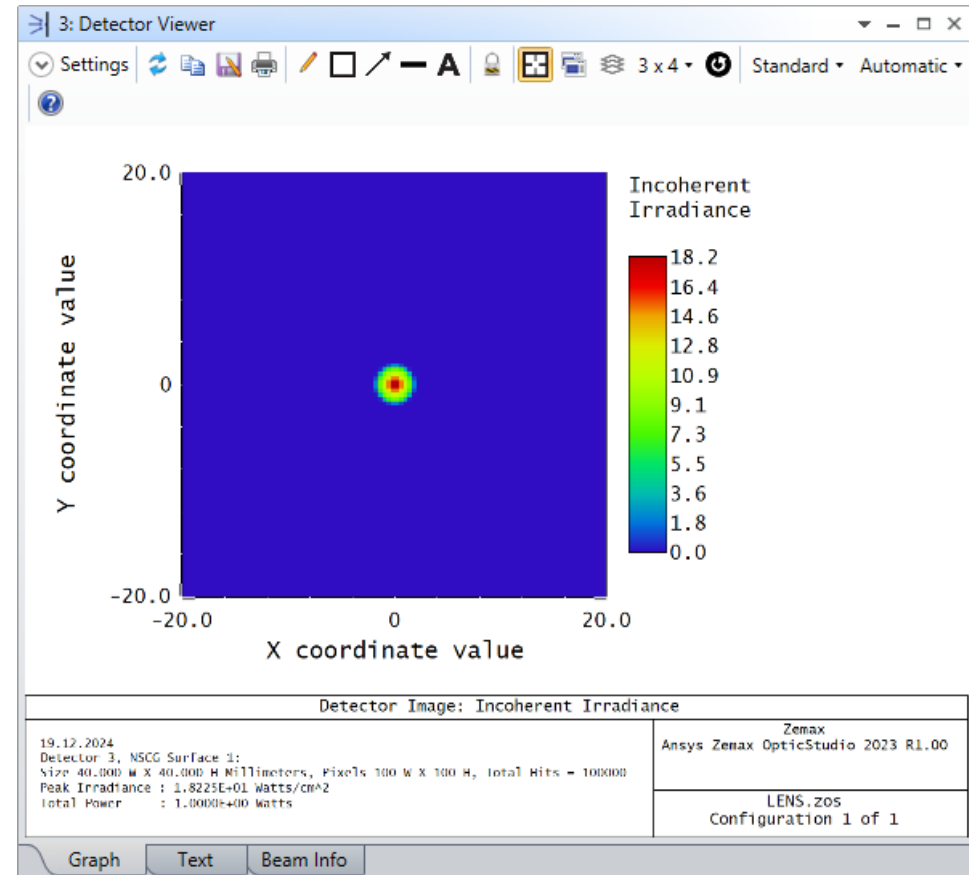
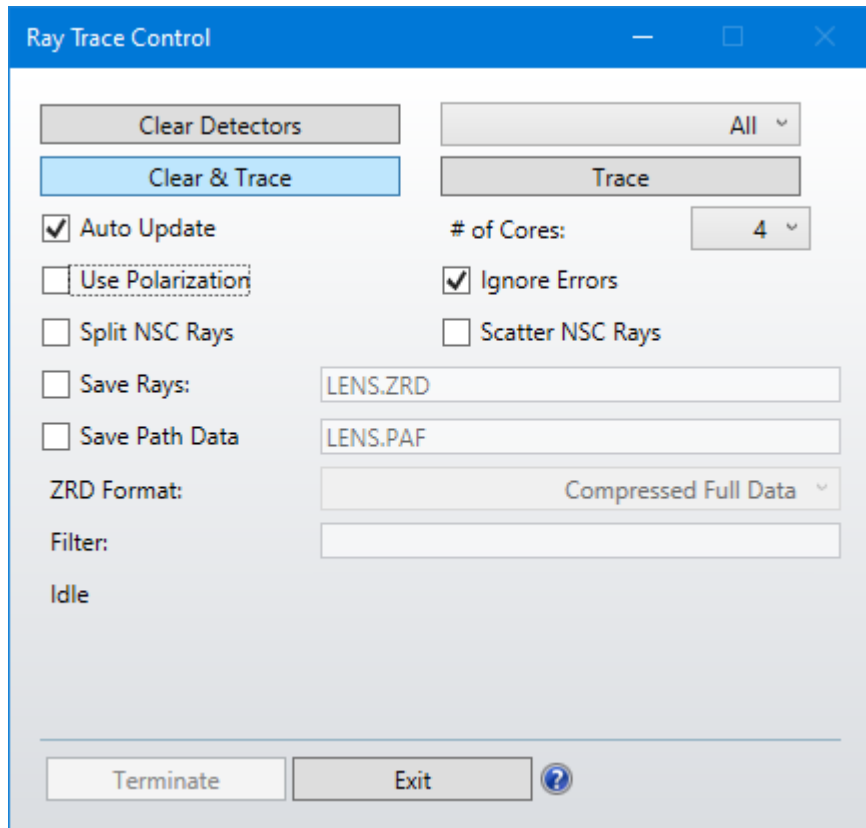
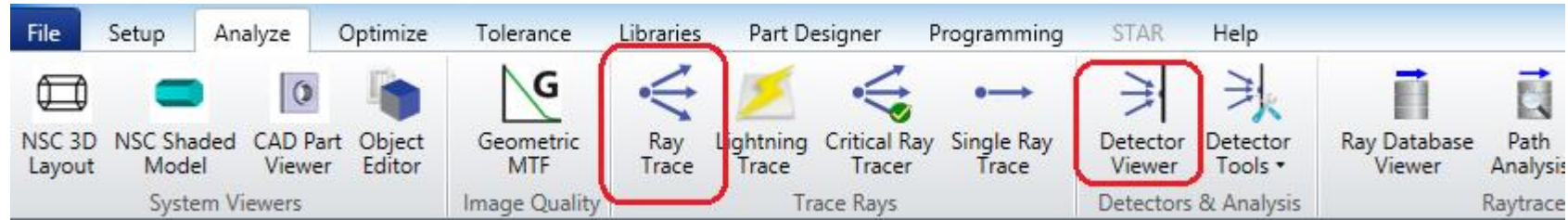
Color 3 (detector displays false color)

Example 1: Layout

Object Type	Comment	Ref Object	Inside Of	X Position	Y Position	Z Position	Tilt About X	Tilt About Y	Tilt About Z	Material	X Half Width	Y Half Width	# X Pixels	# Y Pixels	Data Type	Color
1 Source Ellipse ▾		0	0	0.000	0.000	0.000	0.000	0.000	0.000	-	20	1E+05	1.000	0	0	12.000
2 Standard Lens ▾		0	0	0.000	0.000	20.000	0.000	0.000	0.000	BK7	100.000	0.000	20.000	20.000	6.000	-80.000
3 Detector Rectangle ▾		0	0	0.000	0.000	120.000 V	0.000	0.000	0.000		20.000	20.000	100	100	0	3



Example 1: Ray Tracing



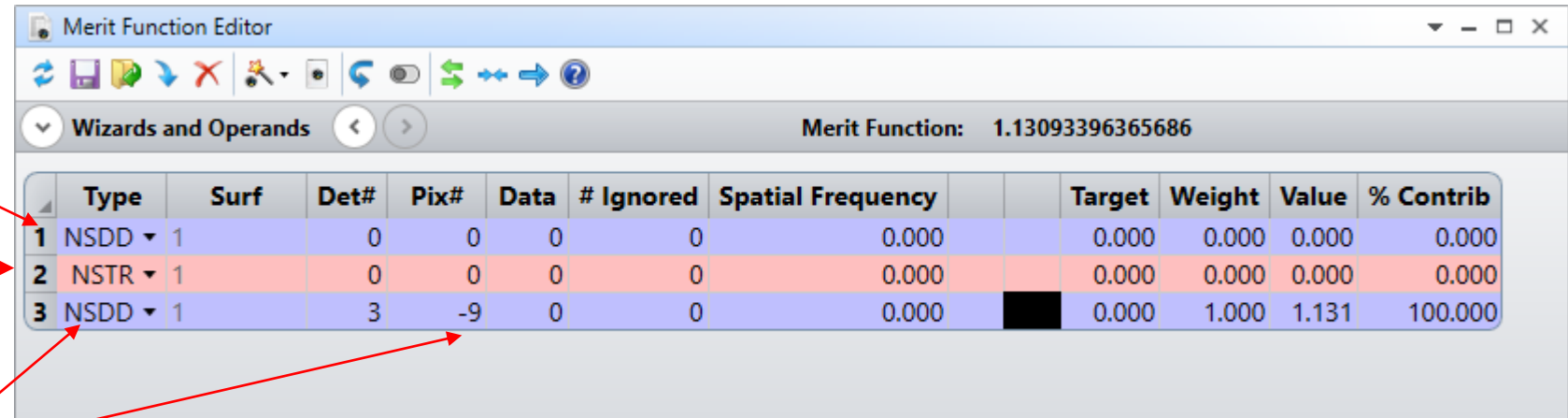
Example 1: Optimization

The aim is to put detector at a location where we have minimum rms spot size

Clear detector

Start ray tracing

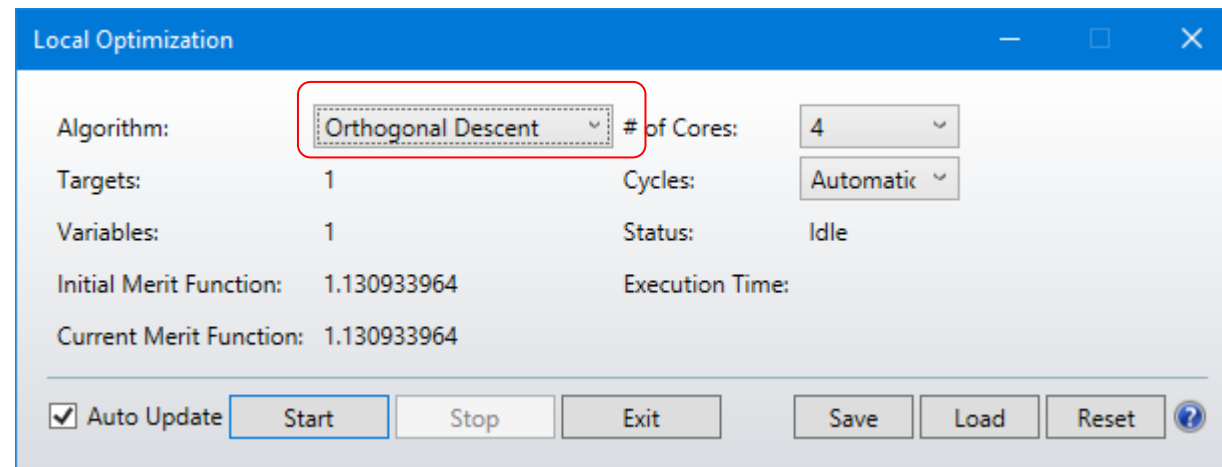
Obtain minimum spot size



Merit Function Editor

Wizards and Operands Merit Function: 1.13093396365686

	Type	Surf	Det#	Pix#	Data	# Ignored	Spatial Frequency	Target	Weight	Value	% Contrib
1	NSDD	1	0	0	0	0	0.000	0.000	0.000	0.000	0.000
2	NSTR	1	0	0	0	0	0.000	0.000	0.000	0.000	0.000
3	NSDD	1	3	-9	0	0	0.000		1.000	1.131	100.000



Local Optimization

Algorithm: **Orthogonal Descent** # of Cores: 4

Targets: 1 Cycles: Automatic

Variables: 1 Status: Idle

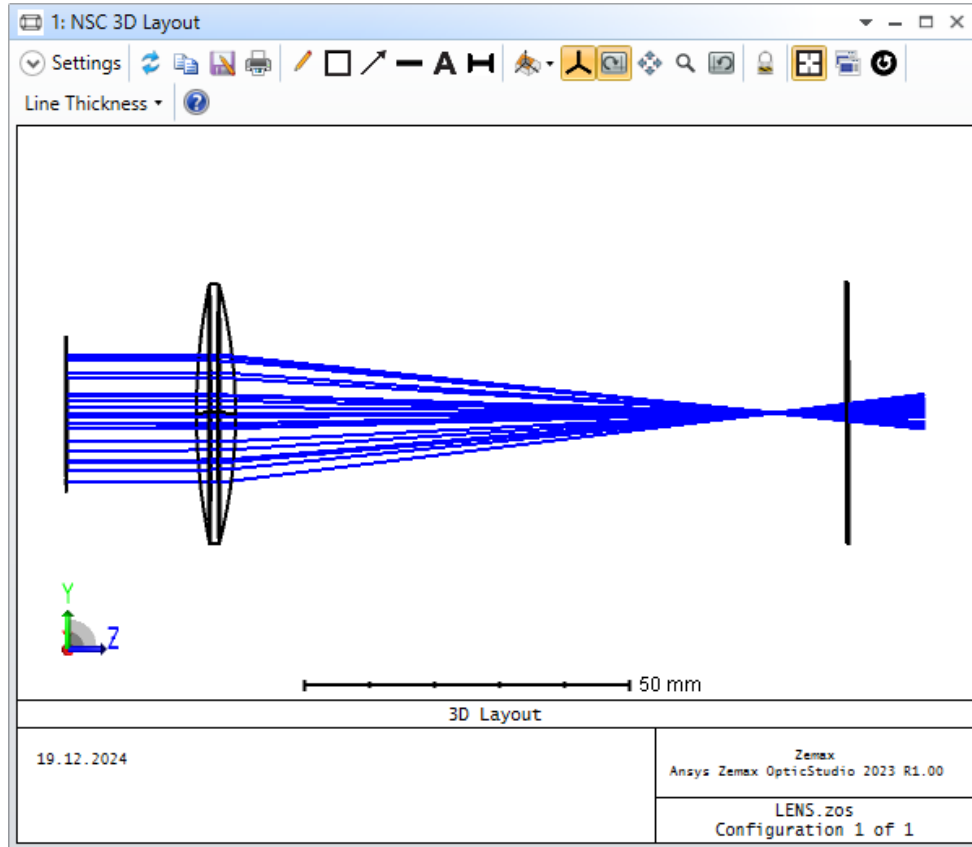
Initial Merit Function: 1.130933964 Execution Time:

Current Merit Function: 1.130933964

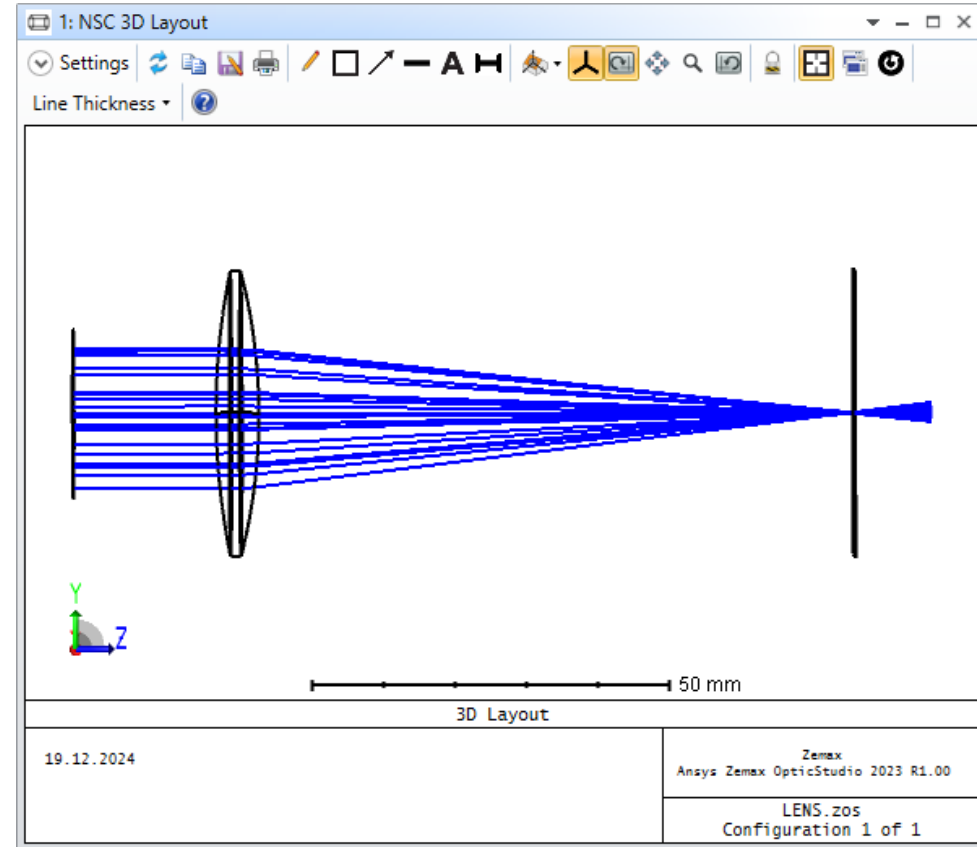
Auto Update Start Stop Exit Save Load Reset

Example 1: Results

Z Position of detector = 120 mm
Before optimization



Z Position of detector = 108.7 mm
After optimization

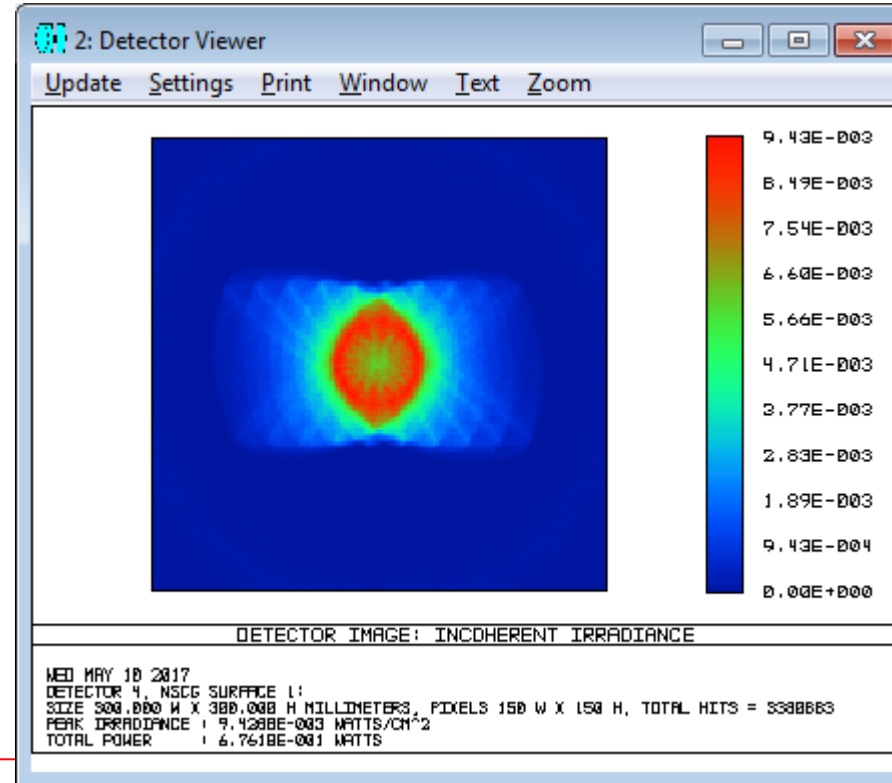
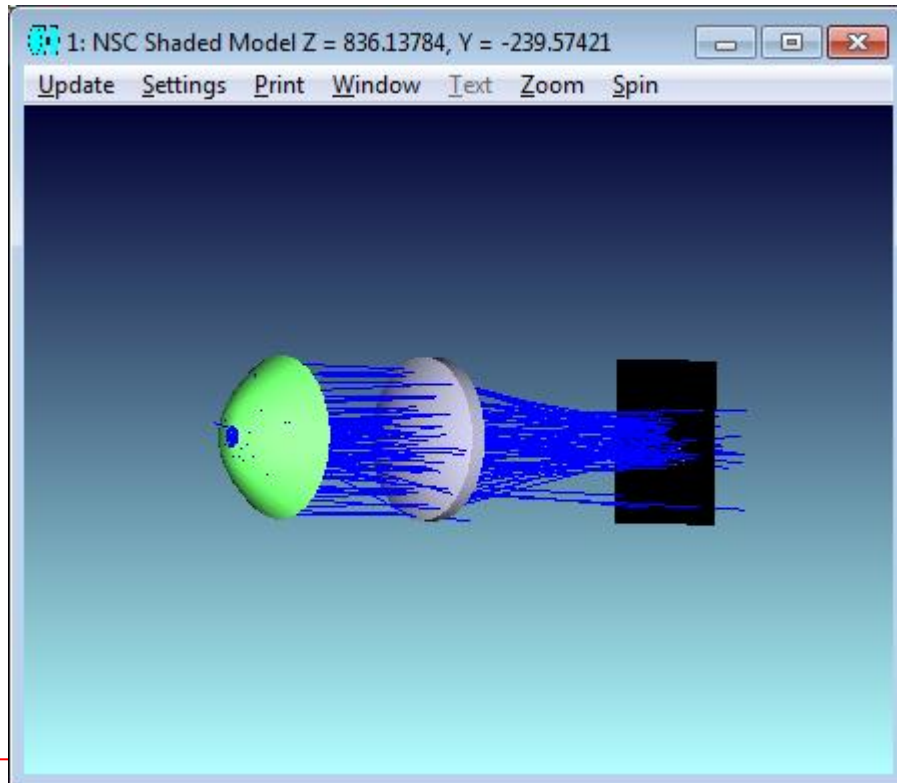


Example 2: Mirror-Lens-Detector

We will make a non-sequential system with

- a filament source
- a parabolic reflector
- a plano-convex lens
- a rectangular detector

as shown in the layout below:



*** Object1

Standart Surface

Material	Mirror
Radius	100
Conic	-1 (parabola)
Max Aper	150
Min Aper	20 (center hole in the reflector)

*** Object2

Source Filament

Z position	50 (focus of the parabolic reflector)
# Layout Rays	20
# Analysis Rays	5e6
Length	20
Radius	5
Turns	10
Tilt about Y	90 (deg)
X position	-10 (mm)

*** Object4

Standard Lens

Ref Object 3 (before detector)

Z Position 200

Material N-BK7

Radius 1 300

Clear 1 150

Edge 1 150

Thickness 70

Clear 2 150

Edge 2 150

*** Object5

Detector Rect

Z position 1000

Material Blank (or can be ABSORB or MIRROR)

X Half Width 150

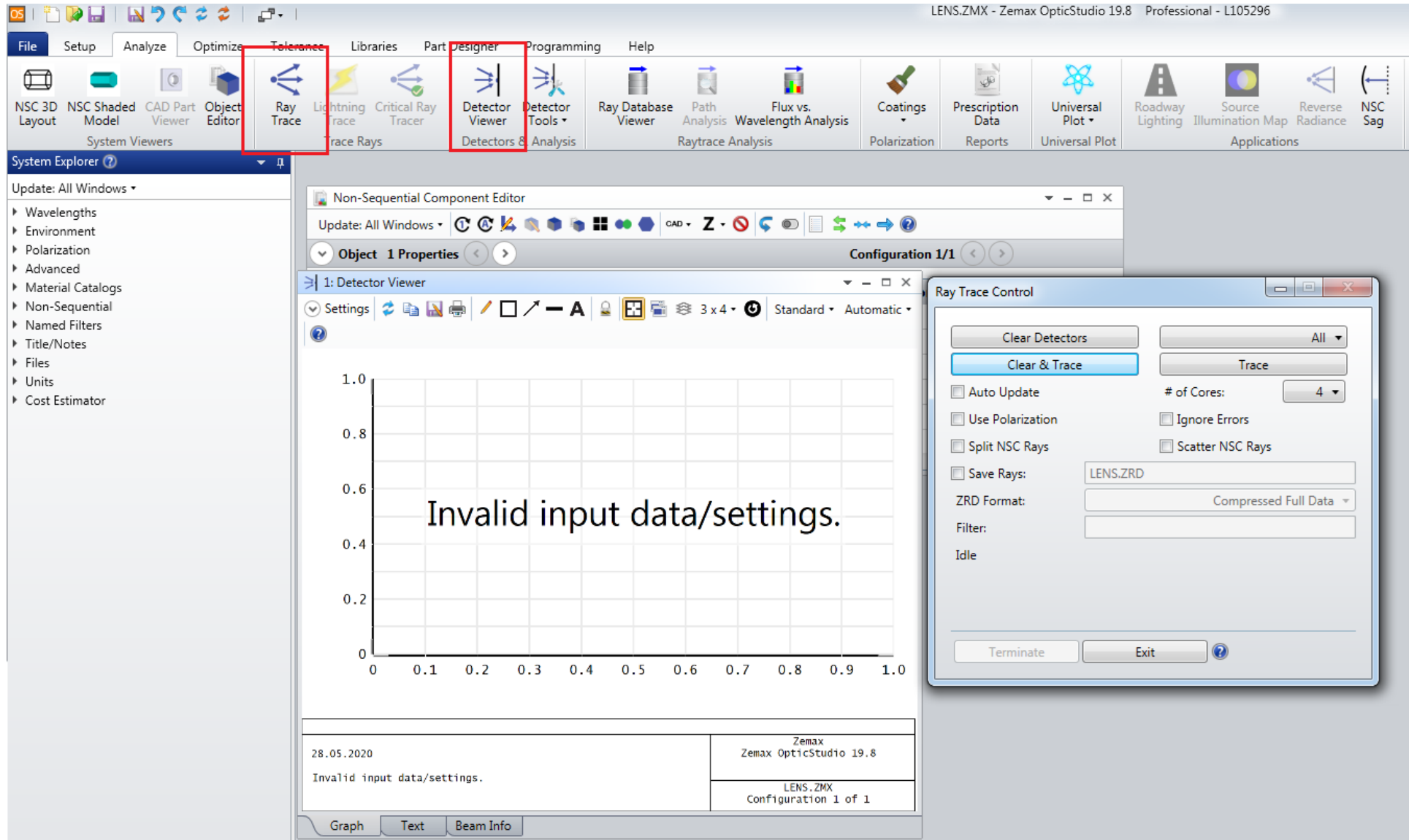
Y Half Width 150

X Pixels 150

Y Pixels 150

Color 1 (detector displays inverse greyscale)

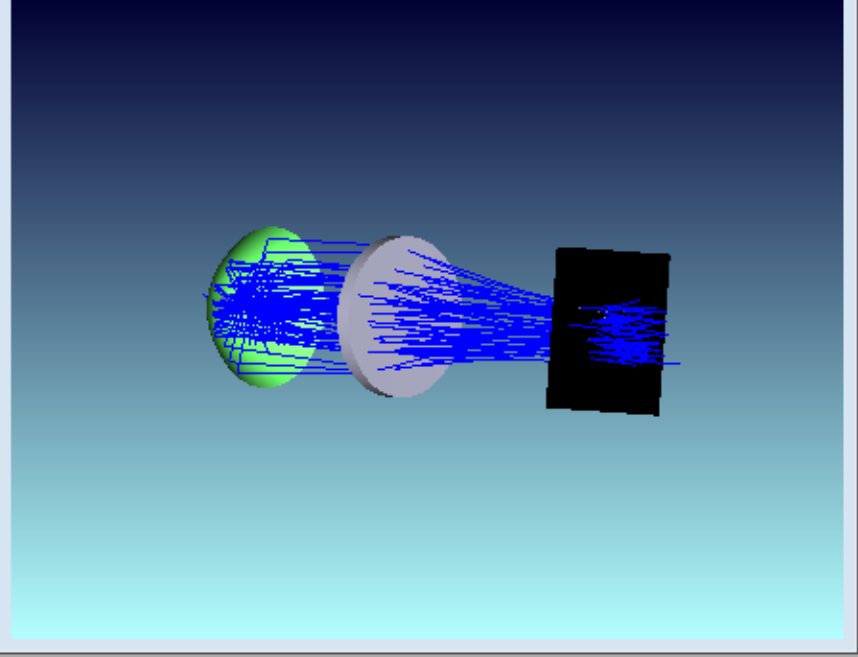
In the analysis you should use **Detector Viewer** and **Ray Trace** buttons.



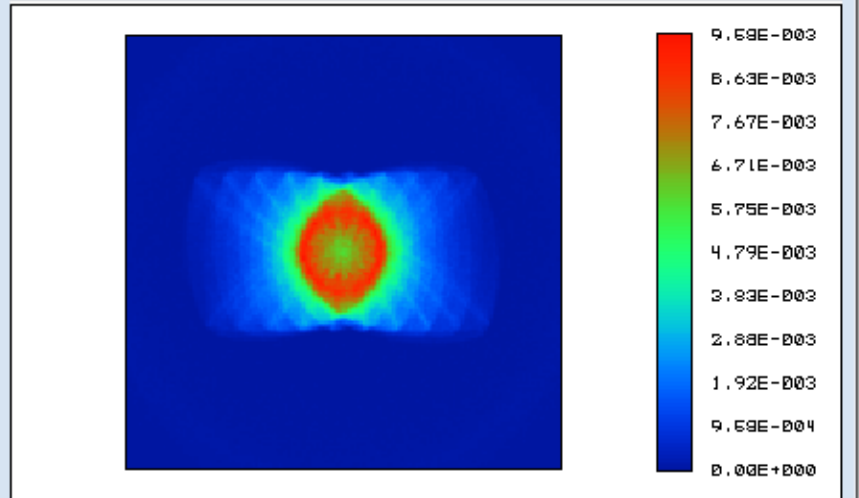
Non-Sequential Component Editor

Object Type	Tilt About Z	Material	X Half Width	Y Half Width	# X Pixels	# Y Pixels
1 Standard ..	0.000	MIRROR	100.000	-1.000	150.000	20.000
2 Source Fi..	0.000	-	100	5000000	1.000	0
3 Standard ..	0.000	N-BK7	300.000	0.000	150.000	150.000
4 Detector ..	0.000		150.000	150.000	150	150
5 Null Object	0.000	-				

1: NSC Shaded Model



2: Detector Viewer



DETECTOR IMAGE: INCOHERENT IRRADIANCE

MED MAY 10 2017
 DETECTOR 4, NSCG SURFACE 1:
 SIZE 300.000 W X 300.000 H MILLIMETERS, PIXELS 150 W X 150 H, TOTAL HITS = 3379270
 PEAK IRRADIANCE : 9.6942E-003 WATTS/CM^2
 TOTAL POWER : 6.7596E-003 WATTS

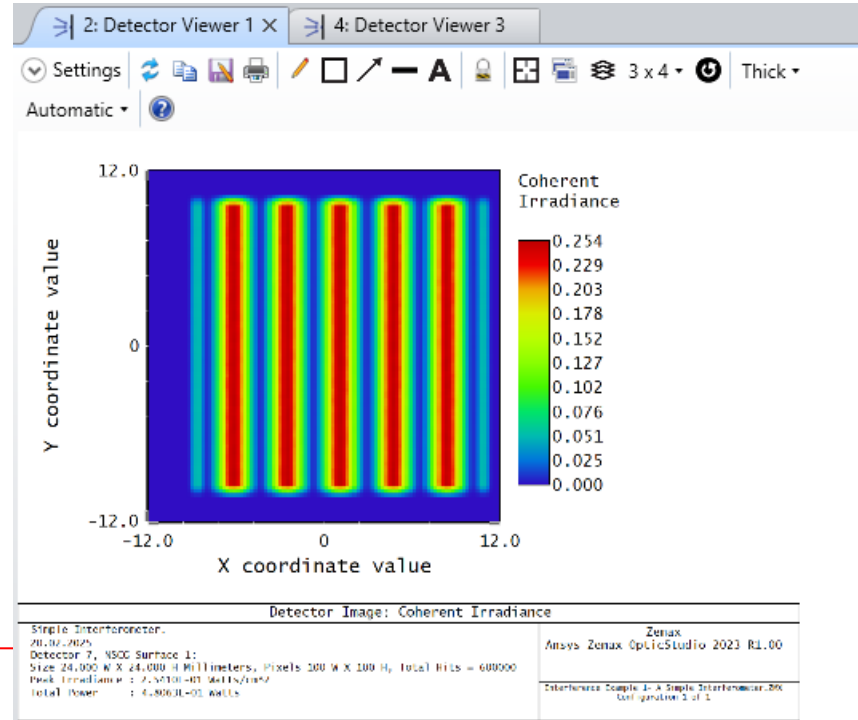
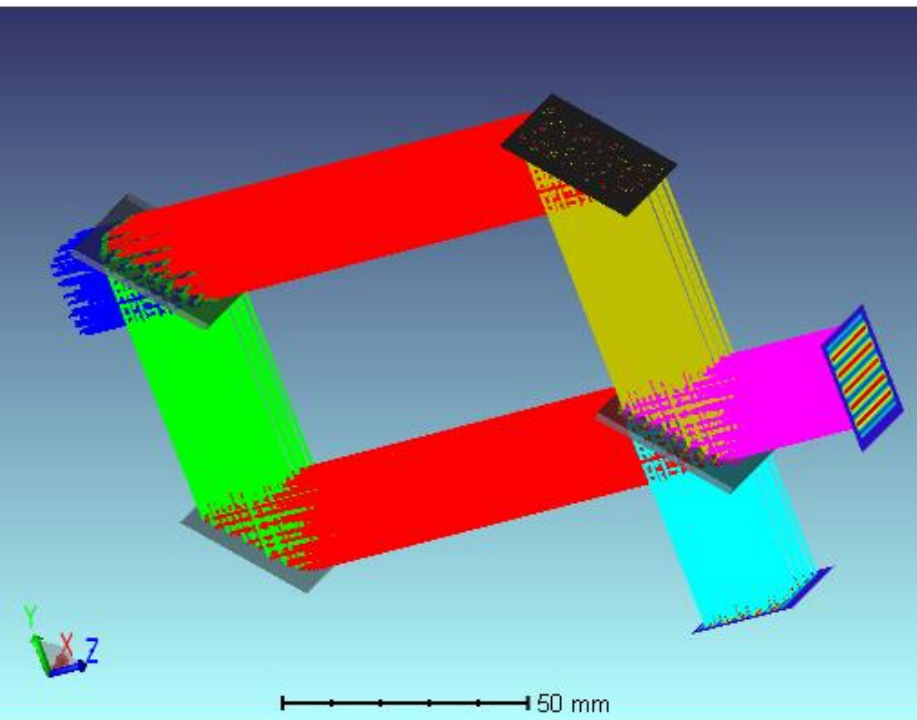
Example 3: Simple Interferometer

Non-Sequential Component Editor

Update: All Windows

Object 7 Properties Configuration 1/1

Object Type	Comment	Ref	Ins	X Position	Y Position	Z Position	Tilt About X	Tilt About Y	Tilt About Z	Material	X Half Width	Y Half Width	# X Pixels	# Y Pixels
Source Rectangle		0	0	0.000	0.000	0.000	0.000	0.000	0.000	-	100	3E+05	1.000	0
Polygon Object	SPLITTER.POB	0	0	0.000	0.000	20.000	-45.000	0.000	0.000	BK7	16.000	1		
Rectangle		0	0	0.000	-60.000	20.000	-45.005	0.000	0.000	MIRROR	15.000	15.000		
Rectangle		0	0	0.000	0.000	120.000	-45.000	0.000	0.000	MIRROR	15.000	15.000		
Polygon Object	SPLITTER.POB	0	0	0.000	-60.000	120.000	-225.000	0.000	0.000	BK7	16.000	1		
Detector Rectangle		0	0	0.000	-60.000	160.000	0.000	0.000	-90.000	ABSORB	12.000	12.000	100	100
Detector Rectangle		0	0	0.000	-100.000	120.000	90.000	0.000	-90.000	ABSORB	12.000	12.000	100	100

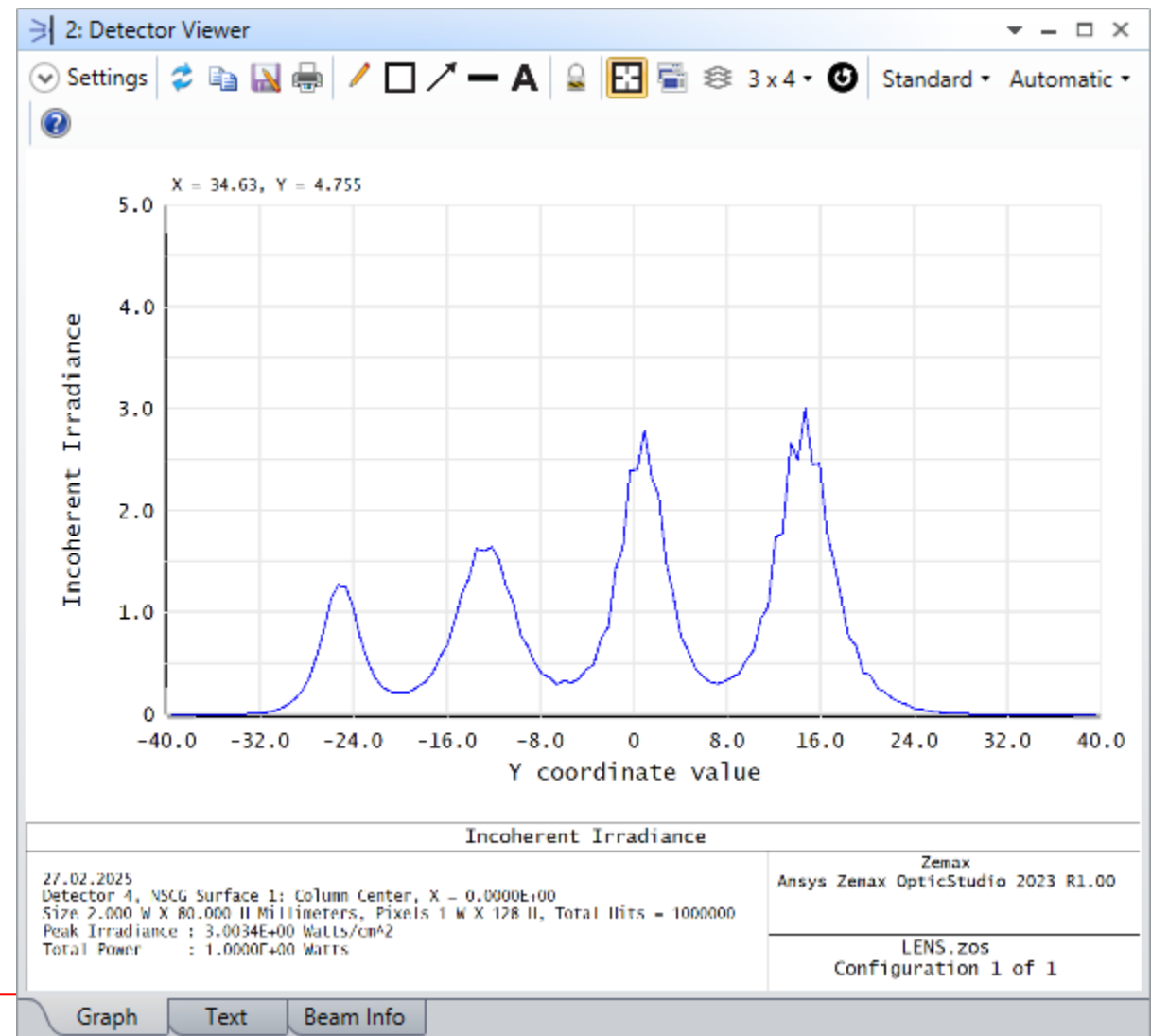
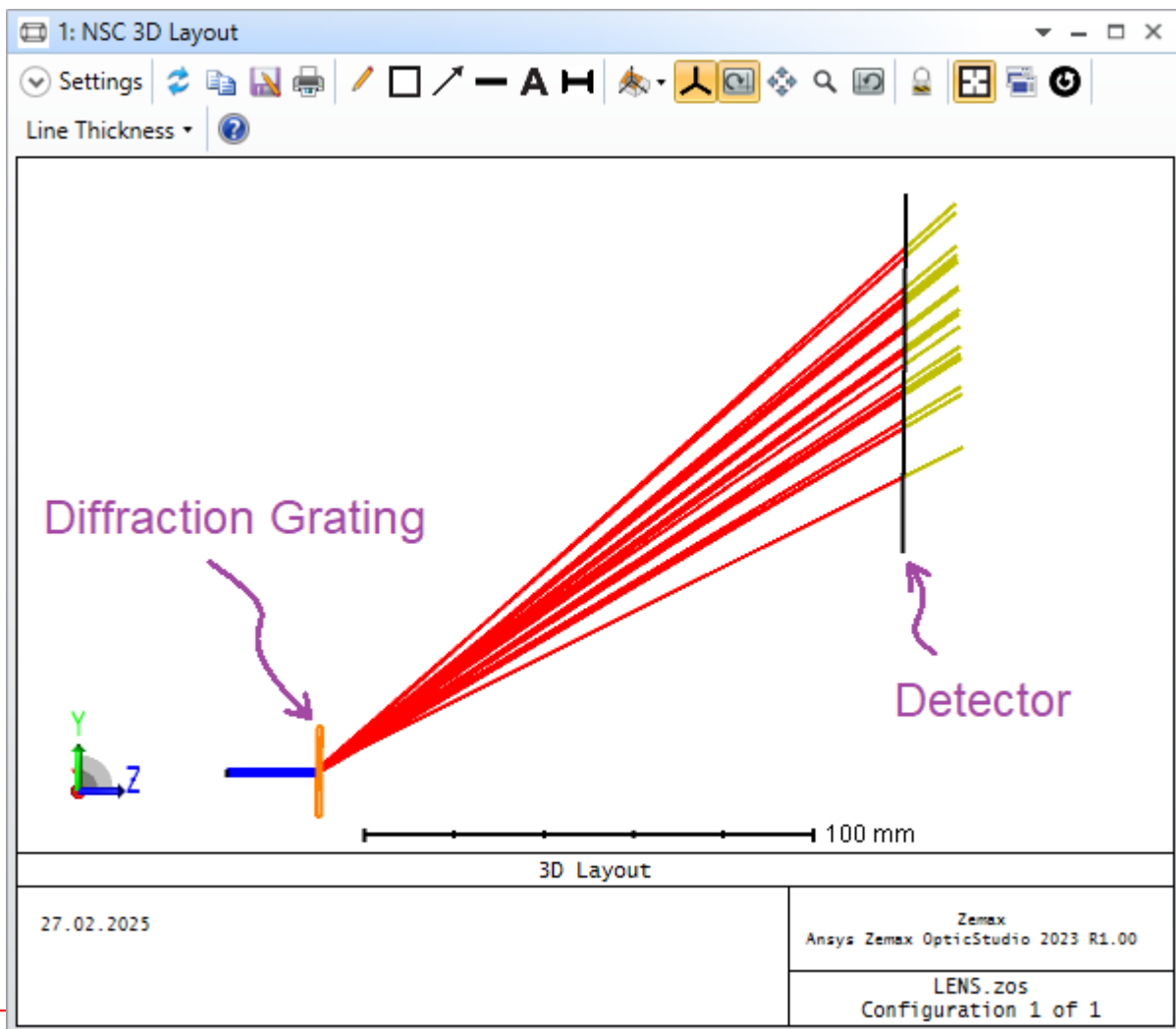


Modify the system

- Elliptic source
- using point source. (first collimate point source using a suitable lens from lens catalog)

Example 4: Simple Spectrometer

Object Type	Comment	Ref Object	Inside Of	X Position	Y Position	Z Position	Tilt About X	Tilt About Y	Tilt About Z	Material	Radius 1	Conic 1	Clear 1	Edge 1	Thickness	Radius 2	Conic 2	Clear 2
1 Source Ellipse		0	0	0.000	0.000	0.000	0.000	0.000	0.000	-	10	0	1.000	0	0	1.000	1.000	0.000
2 Source Ellipse		0	0	0.000	0.000	0.000	0.000	0.000	0.000	-	10	1E+06	1.000	0	0	1.000	1.000	0.000
3 Diffraction Grating		0	0	0.000	0.000	20.000	0.000	0.000	0.000		0.000	0.000	10.000	10.000	1.000	0.000	0.000	10.000
4 Detector Rectangle		0	0	0.000	90.000	150.000	0.000	0.000	0.000		1.000	40.000	1	128	0	0	0	0



Diffraction Grating

is a useful device for analyzing light sources, consists of a large number of equally spaced parallel slits. A transmission grating can be made by cutting parallel lines on a glass plate with a precision ruling machine.

Grating equation: $d\sin(\theta) = m\lambda$

$$d = 1/n$$

n = number of lines per length (e.g. 1/600 mm)

$m = 0, \pm 1, \pm 2, \dots$ (order)

λ = wavelength

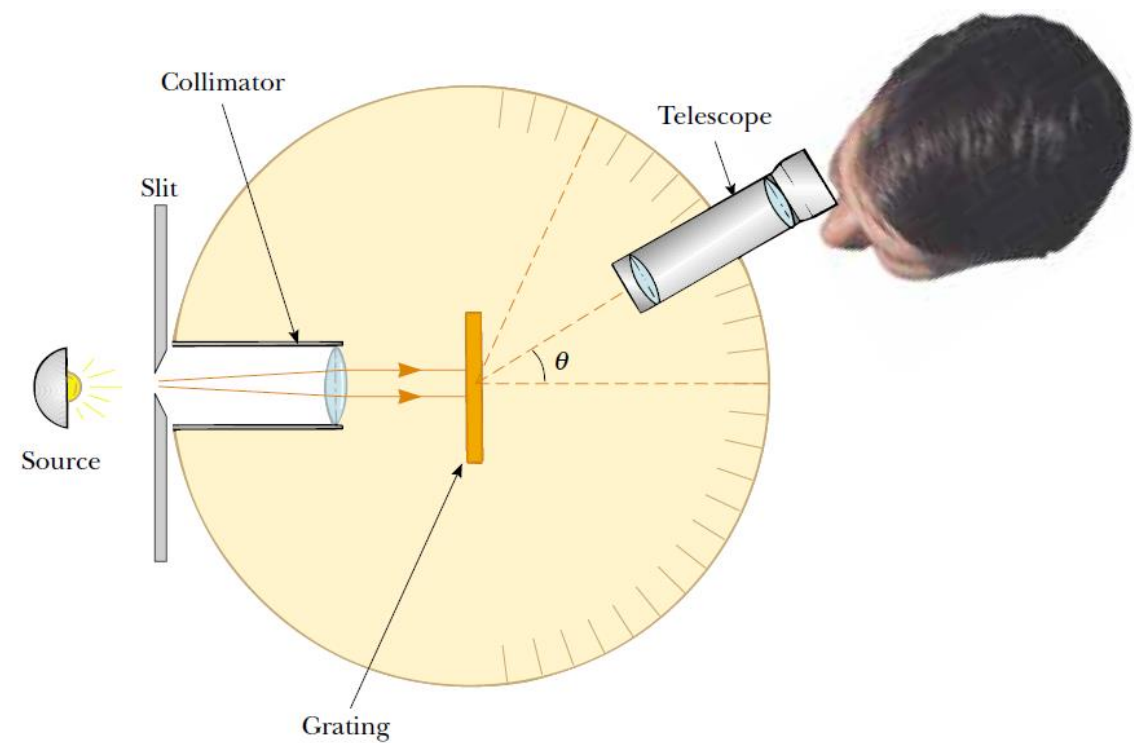
Example: Monochromatic light from a helium-neon laser (632.8 nm) is incident normally on a diffraction grating containing 600 lines/mm. Find the angles at which the first, second and third-order maxima are observed.

$$d = 1/600 = 1667 \text{ nm}$$

$$\sin(\theta_1) = \lambda/d = 0.380 \quad \rightarrow \quad \theta_1 = 22.1^\circ$$

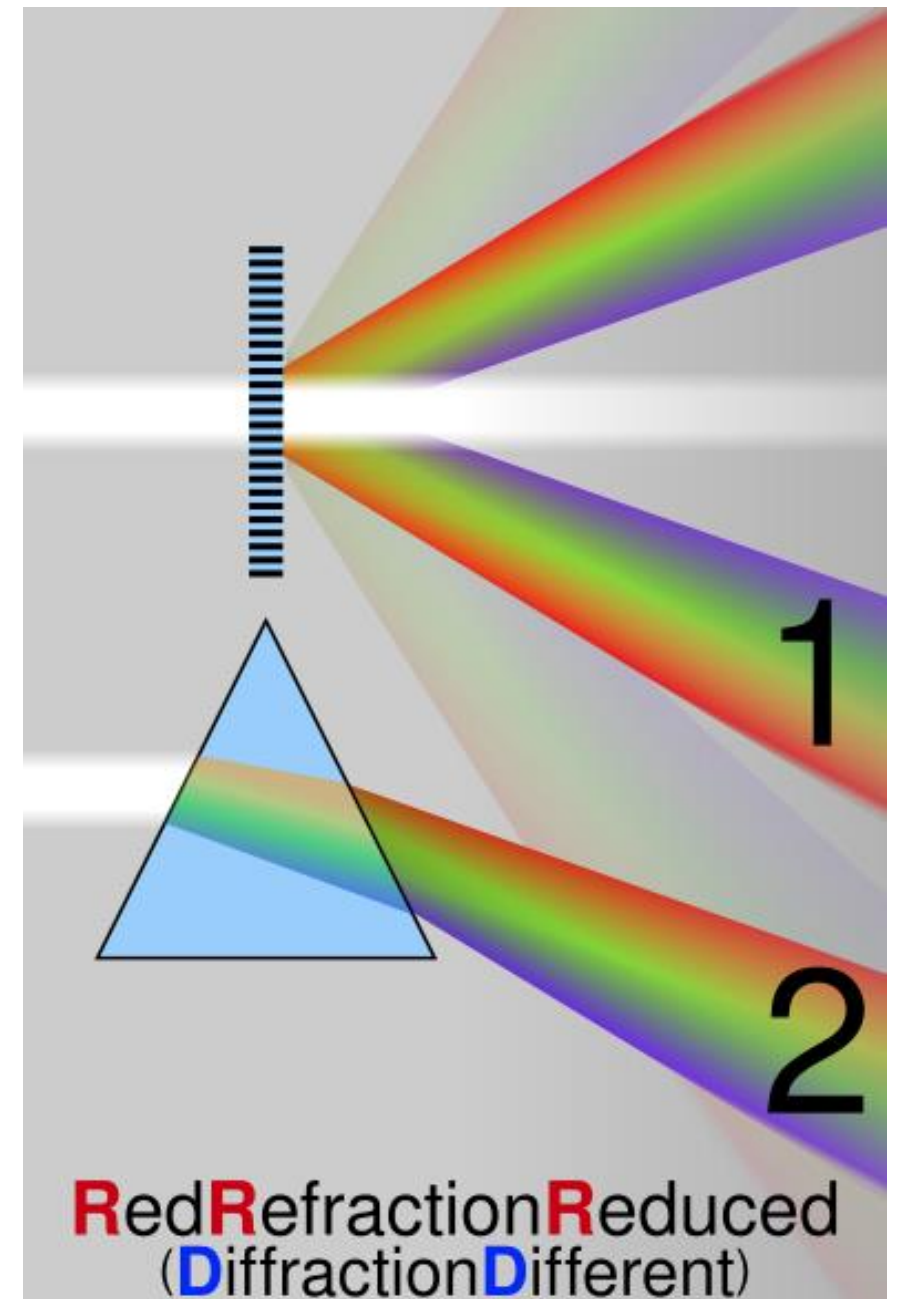
$$\sin(\theta_2) = 2\lambda/d = 0.759 \quad \rightarrow \quad \theta_2 = 49.4^\circ$$

$$\sin(\theta_3) = 3\lambda/d = 1.139 \quad \rightarrow \quad \theta_3 = 90^\circ - 29.9^\circ \mathbf{i} \quad \text{[not realistic]}$$



Comparison of the spectra obtained from a diffraction grating by diffraction (1), and a prism by refraction (2). Longer wavelengths (red) are diffracted more, but refracted less than shorter wavelengths (violet).

https://en.wikipedia.org/wiki/Diffraction_grating



Resolving power:

For two nearly equal wavelengths λ_1 and λ_2 between which a diffraction grating can just barely distinguish, the resolving power R of the grating is defined as: $R = \lambda/\Delta\lambda$

where $\lambda = (\lambda_1 + \lambda_2)/2$ and $\Delta\lambda = \lambda_2 - \lambda_1$.

Thus, a grating that has a high resolving power can distinguish small differences in wavelength. If N lines of the grating are illuminated, it can be shown that the resolving power in the m th-order diffraction is: $R = Nm$

Example: When an element is raised to a very high temperature, the atoms emit radiation having discrete wavelengths. The set of wavelengths for a given element is called its atomic spectrum. Two strong components in the atomic spectrum of sodium have wavelengths of 589.00 nm and 589.59 nm. (See next page)

(a) What must be the resolving power of a grating if these wavelengths are to be distinguished?

$$R = \frac{\lambda}{\Delta\lambda} = 999$$

(b) To resolve these lines in the second-order spectrum, how many lines of the grating must be illuminated?

$$N = \frac{R}{m} = 500 \text{ lines}$$

